# STORMWATER MANAGEMENT DRAINAGE REPORT

# (PRELIMINARY)

Center Street Market

**Crooked Can Brewery, LLC** 

City of Hilliard

8/6/2018

REGISTERED ENGINEER E-76866 DATE



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## **Project Information**

The project is located in Hilliard, Ohio on the corner of Center Street and Wayne Street. The proposed location of the Center Street Market is currently zoned as mixed-use in the historical Old Hilliard District. The proposed 17,000 sf commercial building will be partitioned into multiple sections including a market area, event space, and microbrewery/pub. The 0.740 acre urban site will consist of said commercial building, associated utilities, drives, sidewalk, and pavement improvements. The proposed storm sewer system utilizes underground storage for detention and will discharge directly into an existing storm sewer inlet on the west border of the property. All runoff ultimately discharges into the City of Hilliard storm sewer system.

The purpose of this project is to design a detention system capable of storing the changes in site runoff due to the proposed site construction. Stormwater management for the development will be incorporated into an underground detention system with associated storm sewers and outlet control structure. The detention system will meet the requirements of the City of Hilliard Stormwater Design Manual.

A project location map, soils map and FEMA flood insurance rate map can be found in Appendix A of this report.

## **Existing Drainage Conditions**

The existing site conditions include an open lot consisting of grassy field, gravel areas, and asphalt pavement. The majority of the site currently drains to an existing catch basin located in the center of the lot with small portions of the site draining undetained to the right-of-way. The entirety of the existing site ultimately discharges into the City of Hilliard storm sewer system.

The pre-developed tributary area consists of 0.740 acres of paved parking lot, gravel parking lot, and grass cover, which results in a weighted CN of 92. Additionally, the pre-developed time of concentration (TC) is 10.0 minutes.

NOAA Rainfall data can be found in Appendix A, a pre-developed tributary area map and pre-developed runoff calculations using HydroCAD Version 10.00 by HydroCAD Software Solutions, LLC can be found in Appendix C of this report.

## **Developed Drainage Conditions**

The post-development conditions will be modified as described in the project description of this report. Due to the construction, a storm sewer system will be required. This system will outlet into an underground detention system which will be used for water quantity treatment. The underground detention system will provide storage for the 1-100 year storm events and will discharge into an existing storm sewer inlet located along Center Street. The post-developed tributary area consists of 0.740 acres of impervious area, which results in a weighted CN of 98. Additionally, the post-developed time of concentration (TC) is 10.0 minutes. The proposed tributary map for the post-developed conditions can be found in Appendix D.



#### **General Stormwater Control Narrative**

The critical storm event was calculated by comparing the pre-developed conditions to the post-developed conditions 1-year, 24-hour event using the SCS Type II distribution curve. Detailed Calculations can be found in Appendix B.

- Percentage Increase = 39%
- Critical Storm = 5-Year Event

#### **Stormwater Quantity Control**

Per the City of Hilliard Stormwater Design Manual a 39% increase in runoff assigns the critical storm as the 5-year storm event. The post-developed release rates for storm events 1-5 will release at the pre-developed 1 year event. For every storm event thereafter (10-100 year event) the post-developed release rate will be released at the pre-developed rate.

**Table 3.2.1 Proposed Outlet Structure** 

Invert	Description
930.61	Primary 12" Culvert
930.61	10.0" X 4.4" Rectangular Orifice
931.95	24.0" X 6.0" Rectangular Orifice

<sup>\*</sup>Outlet Structure Detail can be found in Appendix E

**Table 3.2.2 Post-Developed Stormwater Management Summary** 

Storm Event	Allowable Release Rate (cfs)	Post- Developed Flow (cfs)	Detention Basin Release Rate (cfs)	Detention Elevation (feet)	Percent Allowable Peak Discharge
1-Year	1.56	1.97	1.20	931.46	76.92
2-Year	1.56	2.37	1.35	931.64	86.54
5-Year	1.56	2.93	1.54	931.90	98.72
10-Year	3.03	3.38	1.99	932.09	65.68
25-Year	3.70	4.02	2.85	932.25	77.03
50-Year	4.24	4.55	3.49	932.36	82.31
100-Year	4.82	5.11	4.23	932.46	87.76

### **Stormwater Quality Control**

Water quality drawdown per the Ohio EPA NPDES Permit No.: OHCO00005 is not required for this site as the project is less than 1.0 acre of earth disturbance.



#### **Storm Sewer**

An onsite storm sewer system designed for the 2-year design storm and 5-year HGL check storm, per the City of Hilliard Stormwater Design Manual, will be installed to convey stormwater for the development to the proposed retention basin. Additionally, flood routing for storm events up to the 100-year event has been provided overland.

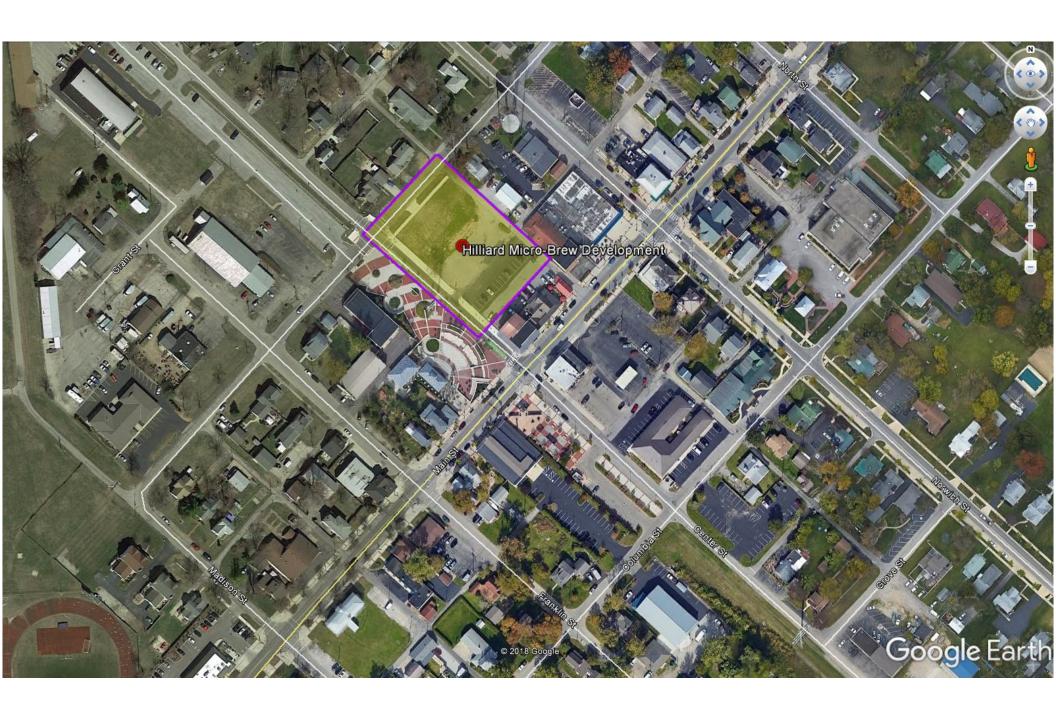
Storm sewer system design calculations can be found in Appendix F, of this report.

## **Summary and Conclusions**

This project has analyzed the pre-developed and post-developed conditions for all storm frequencies (1-100 year) to determine the allowable peak discharge rates and storage requirements. The underground detention system and storm system have been designed to meet or exceed the detention requirements set forth by the City of Hilliard.

Accordingly, we believe the proposed improvements will not adversely affect this site, adjacent property owners, or the City of Hilliard.

# **Appendix A - Project Site Data**





NOAA Atlas 14, Volume 2, Version 3 Location name: Hilliard, Ohio, USA\* Latitude: 40.0346°, Longitude: -83.1602° Elevation: 936.73 ft\*\*

\* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

PDS	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>									
Duration				Averag	e recurrenc	e interval (y	ears)			
Buration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.354</b> (0.319-0.391)	<b>0.421</b> (0.381-0.466)	<b>0.504</b> (0.456-0.557)	<b>0.569</b> (0.514-0.627)	<b>0.652</b> (0.585-0.718)	<b>0.717</b> (0.640-0.787)	<b>0.779</b> (0.692-0.855)	<b>0.844</b> (0.745-0.926)	<b>0.930</b> (0.815-1.02)	<b>0.994</b> (0.864-1.09)
10-min	<b>0.549</b> (0.496-0.608)	<b>0.657</b> (0.595-0.728)	<b>0.784</b> (0.708-0.866)	<b>0.879</b> (0.793-0.968)	<b>0.997</b> (0.895-1.10)	<b>1.09</b> (0.970-1.19)	<b>1.17</b> (1.04-1.29)	<b>1.26</b> (1.11-1.38)	<b>1.37</b> (1.20-1.50)	<b>1.45</b> (1.26-1.59)
15-min	<b>0.673</b> (0.608-0.745)	<b>0.804</b> (0.728-0.890)	<b>0.962</b> (0.870-1.06)	<b>1.08</b> (0.976-1.19)	<b>1.23</b> (1.11-1.36)	<b>1.34</b> (1.20-1.48)	<b>1.46</b> (1.29-1.60)	<b>1.57</b> (1.38-1.72)	<b>1.71</b> (1.50-1.88)	<b>1.81</b> (1.57-1.99)
30-min	<b>0.891</b> (0.805-0.986)	<b>1.08</b> (0.974-1.19)	<b>1.32</b> (1.19-1.46)	<b>1.50</b> (1.36-1.65)	<b>1.74</b> (1.56-1.91)	<b>1.92</b> (1.72-2.11)	<b>2.10</b> (1.87-2.31)	<b>2.29</b> (2.02-2.51)	<b>2.53</b> (2.22-2.78)	<b>2.71</b> (2.36-2.98)
60-min	<b>1.09</b> (0.983-1.20)	<b>1.32</b> (1.20-1.46)	<b>1.65</b> (1.49-1.83)	<b>1.91</b> (1.72-2.10)	<b>2.26</b> (2.02-2.48)	<b>2.53</b> (2.26-2.78)	<b>2.81</b> (2.50-3.09)	<b>3.10</b> (2.74-3.41)	<b>3.50</b> (3.06-3.84)	<b>3.81</b> (3.31-4.18)
2-hr	<b>1.28</b> (1.16-1.41)	<b>1.55</b> (1.40-1.70)	<b>1.93</b> (1.75-2.13)	<b>2.24</b> (2.03-2.46)	<b>2.67</b> (2.40-2.93)	<b>3.02</b> (2.70-3.30)	<b>3.38</b> (3.01-3.69)	<b>3.76</b> (3.32-4.10)	<b>4.29</b> (3.75-4.67)	<b>4.71</b> (4.09-5.14)
3-hr	<b>1.35</b> (1.23-1.48)	<b>1.63</b> (1.49-1.79)	<b>2.04</b> (1.86-2.23)	<b>2.37</b> (2.15-2.59)	<b>2.83</b> (2.56-3.08)	<b>3.20</b> (2.88-3.48)	<b>3.59</b> (3.21-3.91)	<b>4.01</b> (3.56-4.36)	<b>4.59</b> (4.04-4.99)	<b>5.06</b> (4.40-5.50)
6-hr	<b>1.60</b> (1.46-1.76)	<b>1.93</b> (1.76-2.12)	<b>2.39</b> (2.18-2.63)	<b>2.78</b> (2.53-3.04)	<b>3.34</b> (3.01-3.64)	<b>3.79</b> (3.41-4.13)	<b>4.28</b> (3.82-4.65)	<b>4.81</b> (4.25-5.21)	<b>5.55</b> (4.85-6.03)	<b>6.16</b> (5.33-6.69)
12-hr	<b>1.87</b> (1.71-2.07)	<b>2.25</b> (2.05-2.48)	<b>2.78</b> (2.53-3.06)	<b>3.22</b> (2.92-3.55)	<b>3.86</b> (3.48-4.23)	<b>4.39</b> (3.93-4.80)	<b>4.96</b> (4.41-5.42)	<b>5.56</b> (4.91-6.07)	<b>6.44</b> (5.60-7.02)	<b>7.15</b> (6.16-7.80)
24-hr	<b>2.19</b> (2.03-2.37)	<b>2.62</b> (2.43-2.84)	<b>3.22</b> (2.99-3.49)	<b>3.71</b> (3.44-4.01)	<b>4.40</b> (4.06-4.76)	<b>4.97</b> (4.56-5.38)	<b>5.57</b> (5.09-6.02)	<b>6.19</b> (5.62-6.71)	<b>7.07</b> (6.36-7.68)	<b>7.78</b> (6.95-8.47)
2-day	<b>2.54</b> (2.36-2.73)	<b>3.03</b> (2.82-3.27)	<b>3.70</b> (3.44-3.98)	<b>4.24</b> (3.94-4.57)	<b>5.01</b> (4.63-5.39)	<b>5.63</b> (5.18-6.07)	<b>6.27</b> (5.75-6.77)	<b>6.95</b> (6.33-7.51)	<b>7.88</b> (7.11-8.55)	<b>8.63</b> (7.72-9.40)
3-day	<b>2.72</b> (2.54-2.93)	<b>3.25</b> (3.03-3.50)	<b>3.95</b> (3.68-4.25)	<b>4.52</b> (4.20-4.87)	<b>5.31</b> (4.92-5.72)	<b>5.96</b> (5.49-6.41)	<b>6.62</b> (6.07-7.13)	<b>7.31</b> (6.67-7.89)	<b>8.26</b> (7.47-8.94)	<b>9.01</b> (8.09-9.78)
4-day	<b>2.91</b> (2.71-3.13)	<b>3.47</b> (3.23-3.73)	<b>4.21</b> (3.92-4.53)	<b>4.80</b> (4.46-5.16)	<b>5.62</b> (5.21-6.04)	<b>6.29</b> (5.80-6.76)	<b>6.97</b> (6.40-7.50)	<b>7.67</b> (7.01-8.26)	<b>8.63</b> (7.83-9.32)	<b>9.39</b> (8.46-10.2)
7-day	<b>3.47</b> (3.23-3.72)	<b>4.13</b> (3.84-4.43)	<b>4.99</b> (4.64-5.36)	<b>5.69</b> (5.28-6.10)	<b>6.65</b> (6.16-7.14)	<b>7.43</b> (6.86-7.98)	<b>8.23</b> (7.56-8.85)	<b>9.07</b> (8.27-9.77)	<b>10.2</b> (9.25-11.1)	<b>11.1</b> (9.99-12.1)
10-day	<b>3.95</b> (3.71-4.23)	<b>4.69</b> (4.40-5.02)	<b>5.62</b> (5.26-6.00)	<b>6.35</b> (5.94-6.79)	<b>7.37</b> (6.87-7.88)	<b>8.17</b> (7.59-8.74)	<b>8.99</b> (8.32-9.63)	<b>9.84</b> (9.05-10.6)	<b>11.0</b> (10.0-11.8)	<b>11.9</b> (10.8-12.8)
20-day	<b>5.49</b> (5.18-5.83)	<b>6.48</b> (6.12-6.88)	<b>7.61</b> (7.18-8.07)	<b>8.50</b> (8.00-9.01)	<b>9.68</b> (9.09-10.3)	<b>10.6</b> (9.92-11.2)	<b>11.5</b> (10.7-12.2)	<b>12.4</b> (11.5-13.2)	<b>13.6</b> (12.6-14.5)	<b>14.4</b> (13.3-15.4)
30-day	<b>6.87</b> (6.50-7.27)	<b>8.08</b> (7.65-8.55)	<b>9.38</b> (8.87-9.93)	<b>10.4</b> (9.80-11.0)	<b>11.6</b> (11.0-12.3)	<b>12.6</b> (11.9-13.3)	<b>13.5</b> (12.7-14.3)	<b>14.4</b> (13.5-15.3)	<b>15.5</b> (14.5-16.5)	<b>16.4</b> (15.2-17.4)
45-day	<b>8.74</b> (8.30-9.21)	<b>10.3</b> (9.74-10.8)	<b>11.8</b> (11.2-12.4)	<b>12.9</b> (12.3-13.6)	<b>14.4</b> (13.6-15.1)	<b>15.4</b> (14.6-16.3)	<b>16.4</b> (15.5-17.3)	<b>17.4</b> (16.4-18.4)	<b>18.6</b> (17.4-19.6)	<b>19.4</b> (18.1-20.5)
60-day	<b>10.6</b> (10.0-11.1)	<b>12.4</b> (11.7-13.0)	<b>14.1</b> (13.4-14.9)	<b>15.4</b> (14.6-16.3)	<b>17.1</b> (16.2-18.0)	<b>18.3</b> (17.3-19.3)	<b>19.5</b> (18.3-20.6)	<b>20.5</b> (19.3-21.7)	<b>21.9</b> (20.5-23.2)	<b>22.8</b> (21.3-24.2)

<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

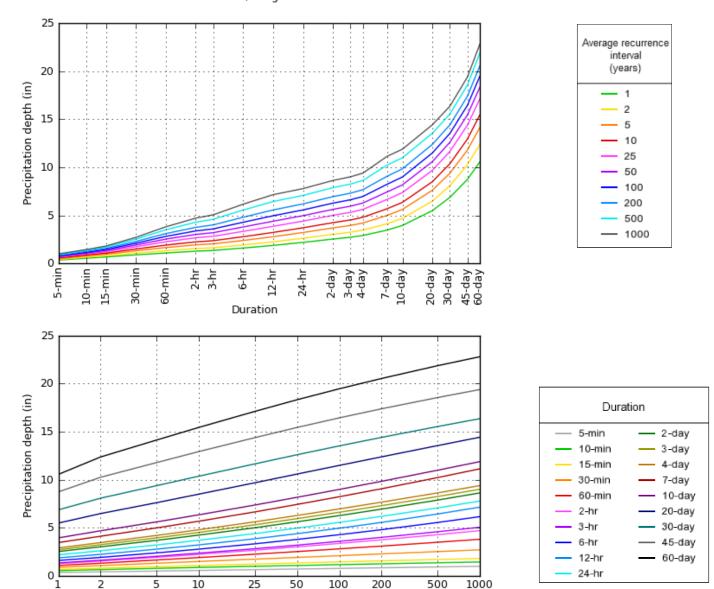
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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#### PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 40.0346°, Longitude: -83.1602°



NOAA Atlas 14, Volume 2, Version 3

Created (GMT): Tue Jul 17 13:30:58 2018

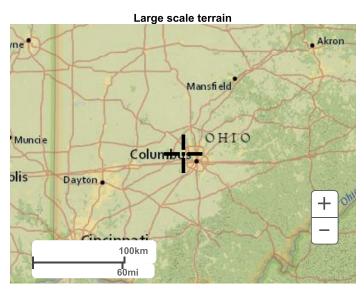
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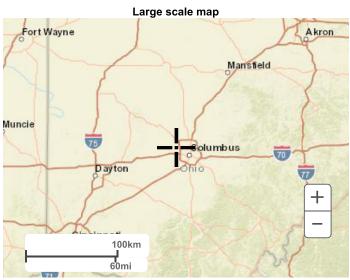
#### Maps & aerials

Small scale terrain

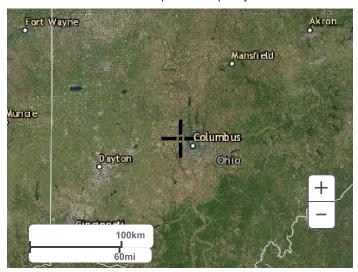
Average recurrence interval (years)







Large scale aerial



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US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

**Disclaimer** 



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Points

#### **Special Point Features**

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

... Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

+ Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Stony Spot

Very Stony Spot

Spoil Area

Wet Spot
Other

#### Water Features

Streams and Canals

#### Transportation

+++ Rails

Interstate Highways

US Routes

Major Roads

Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15.800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Franklin County, Ohio Survey Area Data: Version 15, Oct 5, 2017

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Aug 4, 2014—Aug 27, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
CsA	Crosby-Urban land complex, 0 to 2 percent slopes	0.8	100.0%
Totals for Area of Interest		0.8	100.0%

#### Franklin County, Ohio

#### CsA—Crosby-Urban land complex, 0 to 2 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2w0tj Elevation: 520 to 1,550 feet

Mean annual precipitation: 36 to 44 inches Mean annual air temperature: 48 to 54 degrees F

Frost-free period: 145 to 180 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Crosby and similar soils: 56 percent

Urban land: 35 percent Minor components: 9 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

#### **Description of Crosby**

#### Setting

Landform: Ground moraines, recessionial moraines, water-lain

moraines

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Interfluve, rise

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Silty material or loess over loamy till

#### Typical profile

Ap - 0 to 8 inches: silt loam
BE - 8 to 11 inches: silt loam
Bt1 - 11 to 14 inches: silt loam

2Bt2 - 14 to 28 inches: silty clay loam

2BCt - 28 to 36 inches: loam 2Cd - 36 to 79 inches: loam

#### **Properties and qualities**

Slope: 0 to 2 percent

Depth to restrictive feature: 24 to 40 inches to densic material

Natural drainage class: Somewhat poorly drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Low to

moderately high (0.01 to 0.20 in/hr)

Depth to water table: About 6 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 50 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0

to 2.0 mmhos/cm)

Available water storage in profile: Low (about 5.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: C/D Hydric soil rating: No

#### **Minor Components**

#### Kokomo, drained

Percent of map unit: 5 percent

Landform: Depressions, swales, water-lain moraines Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, dip

Down-slope shape: Linear Across-slope shape: Concave

Hydric soil rating: Yes

#### Celina, eroded

Percent of map unit: 3 percent

Landform: Ground moraines, recessionial moraines, water-lain

moraines

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Crest, head slope, nose

slope, side slope, rise

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Hydric soil rating: No

#### Miamian, eroded

Percent of map unit: 1 percent

Landform: Ground moraines, recessionial moraines, water-lain

moraines

Landform position (two-dimensional): Summit, backslope, shoulder Landform position (three-dimensional): Crest, head slope, nose

slope, side slope, rise

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Hydric soil rating: No

#### **Data Source Information**

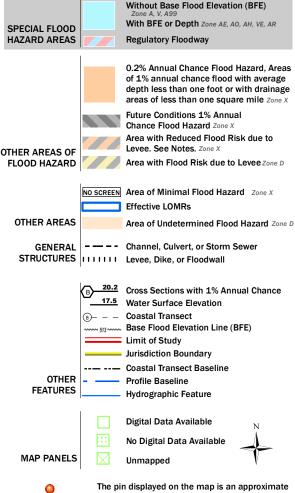
Soil Survey Area: Franklin County, Ohio Survey Area Data: Version 15, Oct 5, 2017

# National Flood Hazard Layer FIRMette



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 8/1/2018 at 10:06:59 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.





# **Appendix B – Critical Storm Calculation**

#### Critical Storm Calculation

Project: Hilliard Microbrew

Job #: 2018.00186 Location: Hilliard, Ohio Date 7/17/18



Calc By: MHS Chk By:

Page 1 of 1

BJM

# Existing Conditions 1 Year, 24 Hour Storm

Project Area	0.740	Acres
Ranfail, P	2.19	Inches
Curve Number, CN	92	
Runoff, Q	1.56	CFS
Total Runoff Volume	0.087	Acre-Feet

#### **Developed Conditions** 1 Year, 24 Hour Storm

Project Area	0.740	Acres
Ranfail, P	2.19	Inches
Curve Number, CN	98	•
Runoff, Q	1.97	CFS
Total Runoff Volume	0.121	Acre-Feet

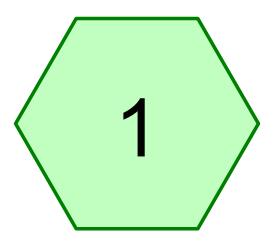
#### Runoff Increse Due to Development

Existing Runoff	0.087 Acre-Feet
Development Runoff	0.121 Acre-Feet
Percent Increase	39 %

#### **Critical Storm**

39% Increase in Runoff; Requires a 5-year critical storm.

- A. Stormwater runoff peak for the 5-year, developed storm will not exceed the stormwater runoff peak for the 1 year, existing storm.
- B. For storms great than the 5-year storm, the developed stormwater runoff will not exceed the existing stormwater runoff peak for each storm. Refer to the stormwater runoff summary for allowable and design peaks.



# Pre-Development Area









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#### **Area Listing (selected nodes)**

Area	CN	Description
 (acres)		(subcatchment-numbers)
0.295	84	Grass (1)
0.224	96	Gravel Parking Lot (1)
0.221	98	Paved Parking Lot (1)
0.740	92	TOTAL AREA

Page 3

#### **Summary for Subcatchment 1: Pre-Development Area**

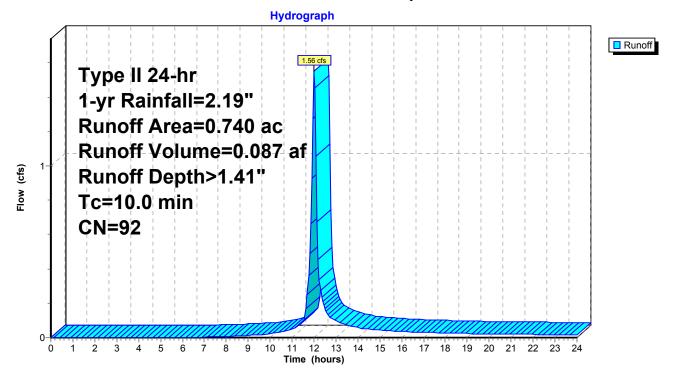
Runoff 1.56 cfs @ 12.01 hrs, Volume= 0.087 af, Depth> 1.41"

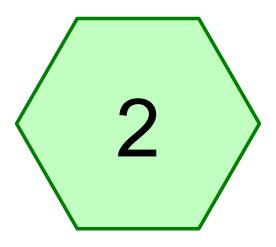
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 1-yr Rainfall=2.19"

	Area (	(ac)	CN	Desc	cription		
*	0.3	221	98	Pave	ed Parking	Lot	
*	0.2	224	96	Grav	el Parking	Lot	
*	0.2	295	84	Gras	S		
	0.	740	92	Weig	hted Aver	age	
	0.	0.519 70.14% Pervious Area					
	0.221 29.86% Impervious Area			6% Imperv	ious Area		
	_					_	
		Leng		Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Minimum TC

**Direct Entry, Minimum TC** 

#### **Subcatchment 1: Pre-Development Area**





# Post-Development Area









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#### **Area Listing (selected nodes)**

Aı	rea C	CN	Description
(acre	es)		(subcatchment-numbers)
0.7	<b>'</b> 40	98	Impervious (2)
0.7	740	98	TOTAL AREA

Page 3

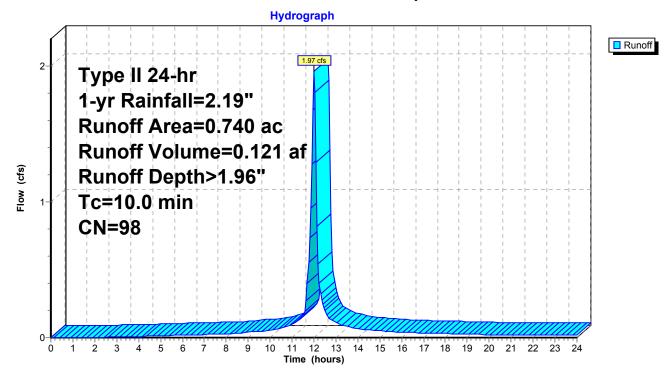
#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 1.97 cfs @ 12.01 hrs, Volume= 0.121 af, Depth> 1.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 1-yr Rainfall=2.19"

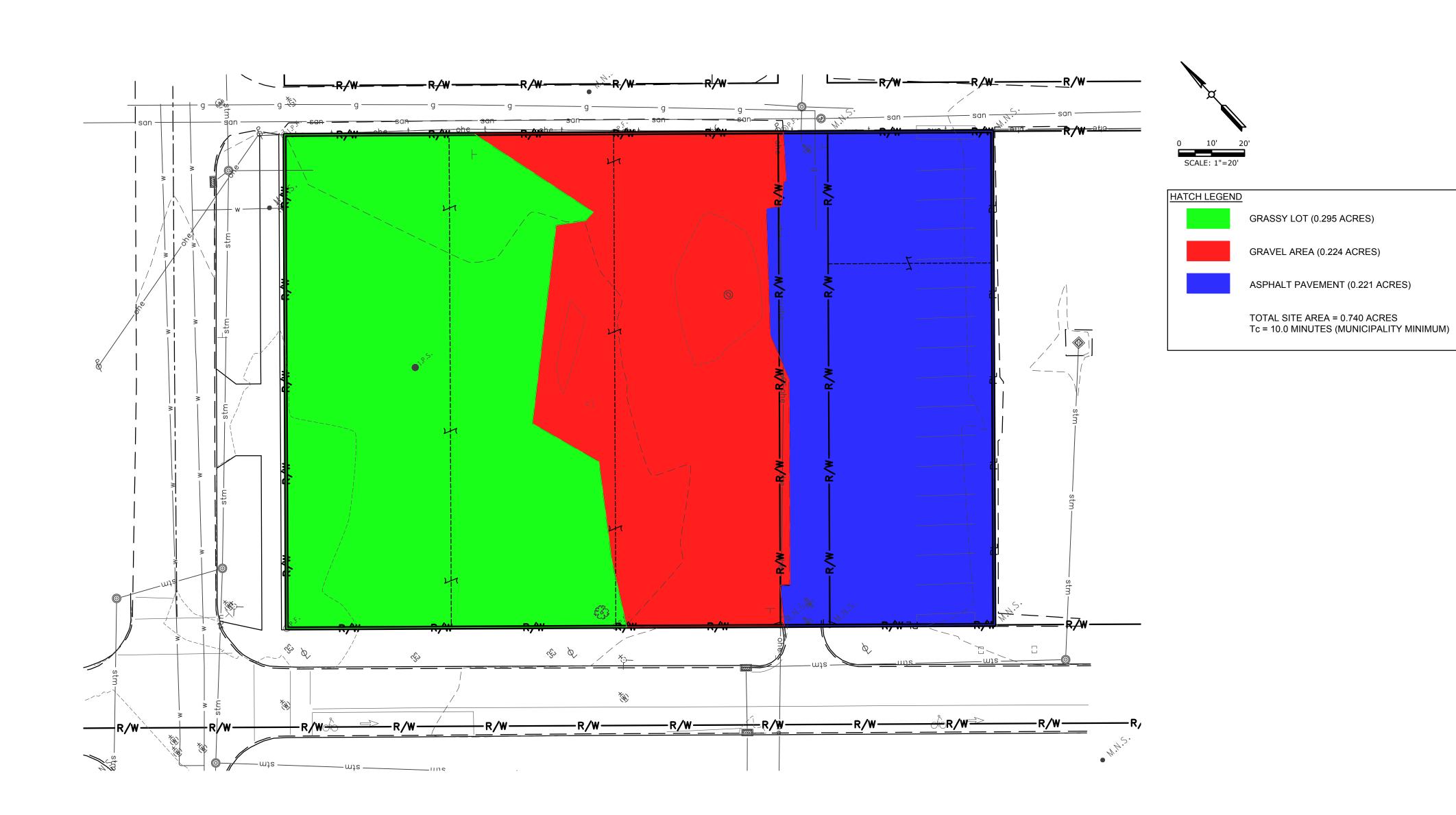
_	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
_	0.	0.740 100.00% Impervious Area					
	Тс	Lengt	h :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·
	10.0						Direct Entry, Minimum TC

#### **Subcatchment 2: Post-Development Area**





# **Appendix C – Pre-Development Calculations**



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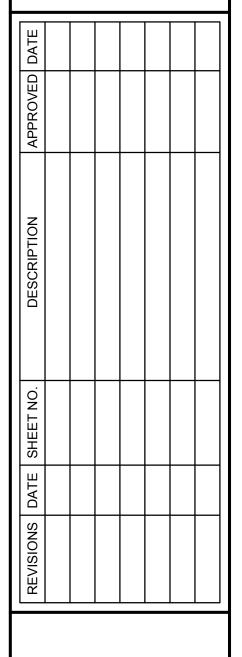
CONSTRUCTION CO.

INC.
INC.
331
331
331
3325

STRUCTUREPOINT
INC.
INC.

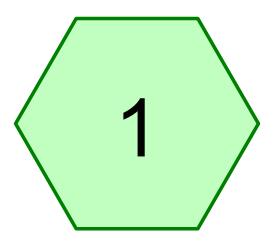
- Vade

PRE-DEVELOPED IRIBUTARY MAP FOR CENTER STREET MARKE HILLIARD, FRANKLIN COUNTY, OH



DATE: 8/1/2018
DRAWN BY: JRP
CHECKED BY: BJM
JOB NUMBER: 2018.00186

PRE



# Pre-Development Area









2018.00186 Drainage
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#### **Area Listing (selected nodes)**

Area	CN	Description
 (acres)		(subcatchment-numbers)
0.295	84	Grass (1)
0.224	96	Gravel Parking Lot (1)
0.221	98	Paved Parking Lot (1)
0.740	92	TOTAL AREA

Page 3

#### **Summary for Subcatchment 1: Pre-Development Area**

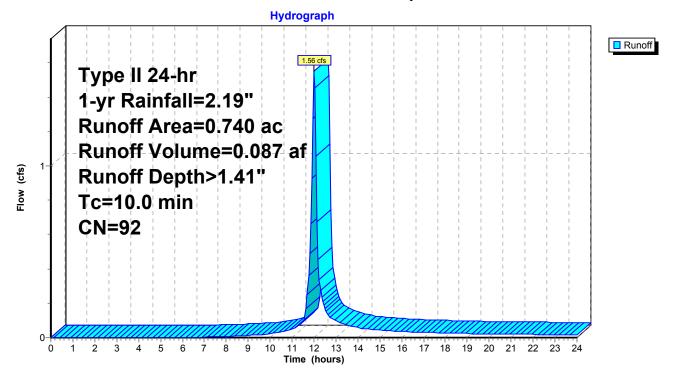
Runoff 1.56 cfs @ 12.01 hrs, Volume= 0.087 af, Depth> 1.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 1-yr Rainfall=2.19"

	Area (	(ac)	CN	Desc	cription		
*	0.3	221	98	Pave	ed Parking	Lot	
*	0.2	224	96	Grav	el Parking	Lot	
*	0.2	295	84	Gras	S		
	0.	740	92	Weig	hted Aver	age	
	0.	519		70.14	4% Pervio	us Area	
	0.3	0.221 29.86% Impervious Area				ious Area	
	_					_	
		Leng		Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Minimum TC

**Direct Entry, Minimum TC** 

#### **Subcatchment 1: Pre-Development Area**



Page 4

#### **Summary for Subcatchment 1: Pre-Development Area**

Runoff = 1.97 cfs @ 12.01 hrs, Volume= 0.111 af, Depth> 1.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-yr Rainfall=2.62"

	Area	(ac)	CN	Desc	Description					
*	0.	221	98	Pave	Paved Parking Lot					
*	0.	224	96	Grav	el Parking	Lot				
*	0.	295	84	Gras	S					
	0.	740	740 92 Weighted Average							
	0.	0.519 70.14% Pervious Area								
	0.221 29.86% Impervious Area			6% Imperv	ious Area					
	_	_								
	Tc	Leng		Slope	Velocity	Capacity	Description			
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	10.0						Direct Entry, Minimum TC			

# Subcatchment 1: Pre-Development Area

# Hydrograph Type II 24-hr 2-yr Rainfall=2.62" Runoff Area=0.740 ac Runoff Depth>1.80" Tc=10.0 min CN=92 On 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 Time (hours)

Page 5

#### **Summary for Subcatchment 1: Pre-Development Area**

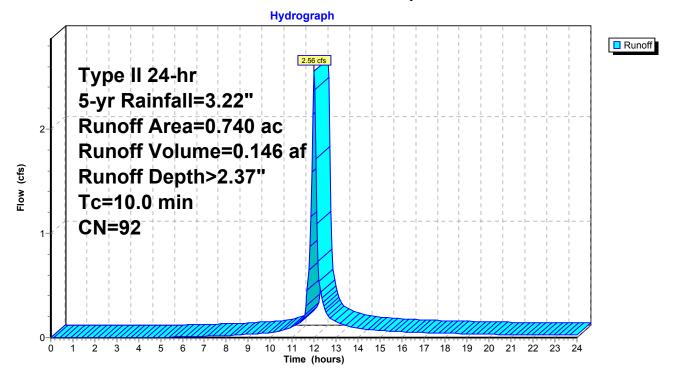
Runoff 2.56 cfs @ 12.01 hrs, Volume= 0.146 af, Depth> 2.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 5-yr Rainfall=3.22"

	Area (	(ac)	CN	Desc	cription		
*	0.3	221	98	Pave	ed Parking	Lot	
*	0.2	224	96	Grav	el Parking	Lot	
*	0.2	295	84	Gras	S		
	0.	740	92	Weig	hted Aver	age	
	0.	519		70.14	4% Pervio	us Area	
	0.3	0.221 29.86% Impervious Area				ious Area	
	_					_	
		Leng		Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Minimum TC

**Direct Entry, Minimum TC** 

#### **Subcatchment 1: Pre-Development Area**



Page 6

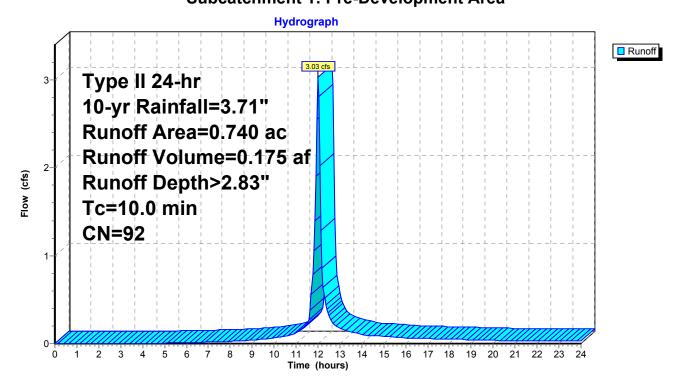
#### **Summary for Subcatchment 1: Pre-Development Area**

Runoff = 3.03 cfs @ 12.01 hrs, Volume= 0.175 af, Depth> 2.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-yr Rainfall=3.71"

_	Area	(ac)	CN	Desc	Description					
*	0.	221	98	Pave	d Parking	Lot				
*	0.	224	96	Grav	el Parking	Lot				
*	0.	295	84	Gras	S					
	0.	740	92	Weig	hted Aver	age				
	0.	519		70.14	4% Pervio	us Area				
	0.221 29.86% Impervious Area			6% Imperv	ious Area					
	т.	Lana	414	Clana	\/alaaitu	Canacity	Description			
	Tc	Leng		Slope	Velocity	Capacity	Description			
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	10.0						Direct Entry, Minimum TC			

#### **Subcatchment 1: Pre-Development Area**



Page 7

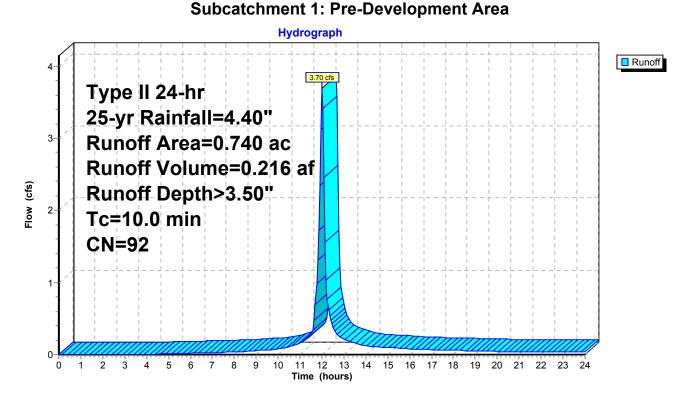
#### **Summary for Subcatchment 1: Pre-Development Area**

Runoff = 3.70 cfs @ 12.01 hrs, Volume= 0.216 af, Depth> 3.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-yr Rainfall=4.40"

	Area	(ac)	CN	Desc	Description					
*	0.	221	98	Pave	Paved Parking Lot					
*	0.	224	96	Grav	el Parking	Lot				
*	0.	295	84	Gras	S					
	0.	740	740 92 Weighted Average							
	0.	0.519 70.14% Pervious Area								
	0.221 29.86% Impervious Area			6% Imperv	ious Area					
	_	_								
	Tc	Leng		Slope	Velocity	Capacity	Description			
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)				
	10.0						Direct Entry, Minimum TC			

#### Nuls at alama at 4. Dua Daviala a maant Anas



Page 8

#### **Summary for Subcatchment 1: Pre-Development Area**

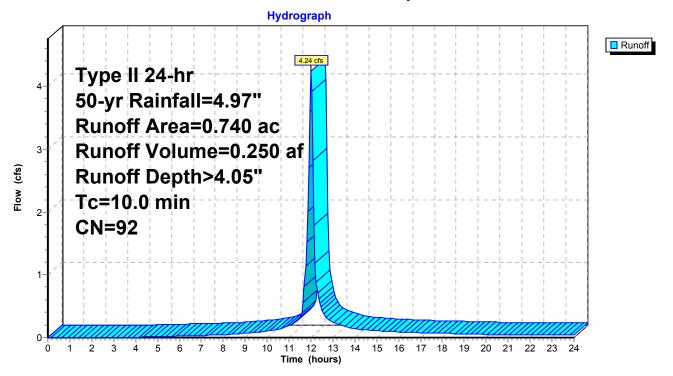
Runoff 4.24 cfs @ 12.01 hrs, Volume= 0.250 af, Depth> 4.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 50-yr Rainfall=4.97"

	Area (	(ac)	CN	Desc	cription		
*	0.3	221	98	Pave	ed Parking	Lot	
*	0.2	224	96	Grav	el Parking	Lot	
*	0.2	295	84	Gras	S		
	0.	740	92	Weig	hted Aver	age	
	0.	519		70.14	4% Pervio	us Area	
	0.3	0.221 29.86% Impervious Area				ious Area	
	_					_	
		Leng		Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Minimum TC

**Direct Entry, Minimum TC** 

#### **Subcatchment 1: Pre-Development Area**



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#### **Summary for Subcatchment 1: Pre-Development Area**

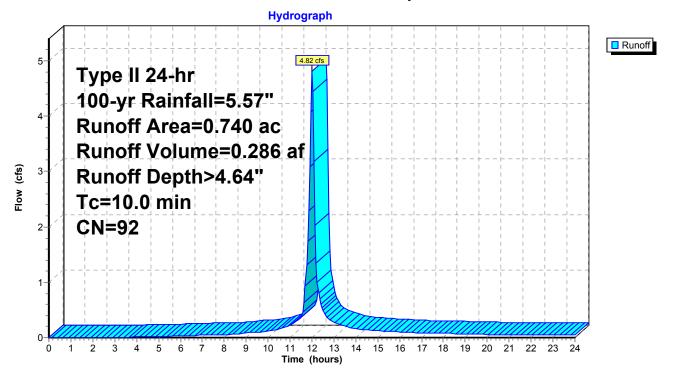
Runoff 4.82 cfs @ 12.01 hrs, Volume= 0.286 af, Depth> 4.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-yr Rainfall=5.57"

	Area (	(ac)	CN	Desc	cription		
*	0.3	221	98	Pave	ed Parking	Lot	
*	0.2	224	96	Grav	el Parking	Lot	
*	0.2	295	84	Gras	S		
	0.	740	92	Weig	hted Aver	age	
	0.	519		70.14	4% Pervio	us Area	
	0.3	0.221 29.86% Impervious Area				ious Area	
	_					_	
		Leng		Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Minimum TC

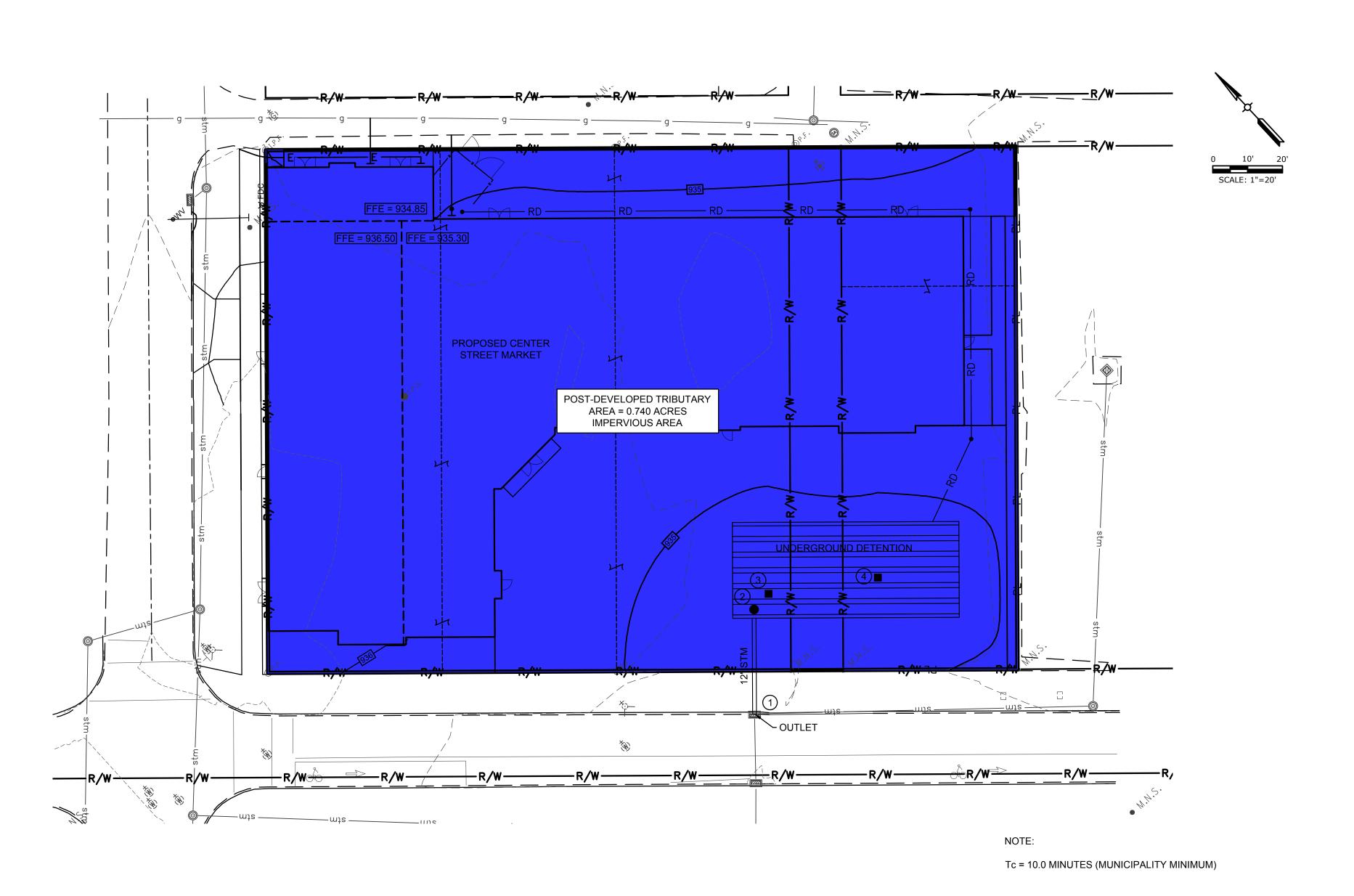
**Direct Entry, Minimum TC** 

#### **Subcatchment 1: Pre-Development Area**





## **Appendix D – Post-Development Calculations**



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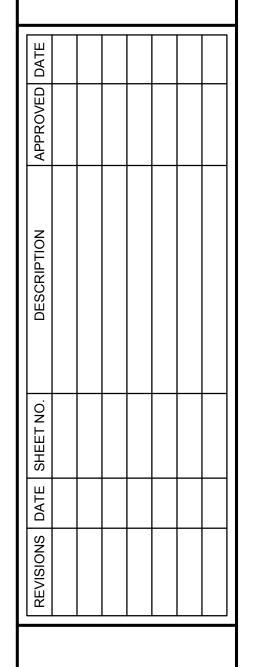
CONSTRUCTION CO.

STRUCTUREPOINT



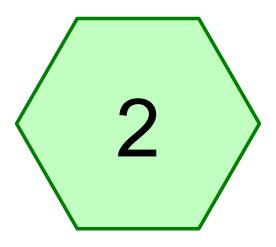
CENTER STREET MARKET

HILLIARD, FRANKLIN COUNTY, OH



DATE: 8/1/2018
DRAWN BY: JRP
CHECKED BY: BJM
JOB NUMBER: 2018.00186

POST



## Post-Development Area









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#### **Area Listing (selected nodes)**

Area		Description
(acres	)	(subcatchment-numbers)
0.740	98	Impervious (2)
0.740	98	TOTAL AREA

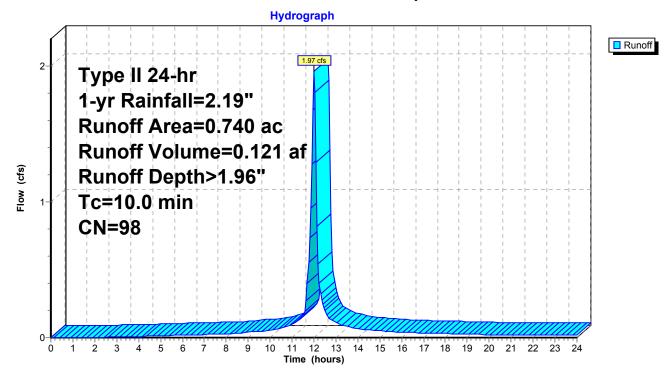
Page 3

#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 1.97 cfs @ 12.01 hrs, Volume= 0.121 af, Depth> 1.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 1-yr Rainfall=2.19"

_	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
_	0.	740		100.	00% Impe	rvious Area	
	Тс	Lengt	h :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·
	10.0						Direct Entry, Minimum TC



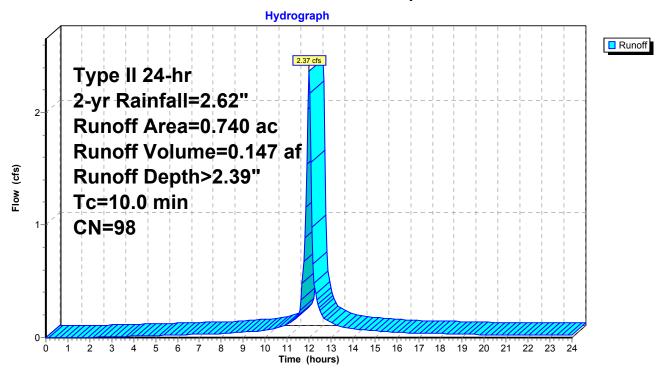
Page 4

#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 2.37 cfs @ 12.01 hrs, Volume= 0.147 af, Depth> 2.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 2-yr Rainfall=2.62"

_	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
_	0.	740		100.	00% Impe	rvious Area	
	Тс	Lengt	h :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·
	10.0						Direct Entry, Minimum TC



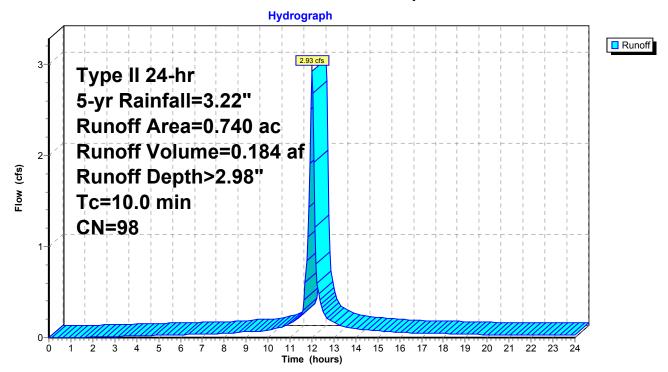
Page 5

#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 2.93 cfs @ 12.01 hrs, Volume= 0.184 af, Depth> 2.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 5-yr Rainfall=3.22"

	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
	0.	740		100.	00% Impe	rvious Area	1
	Тс	Leng	th	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
	10.0						Direct Entry, Minimum TC



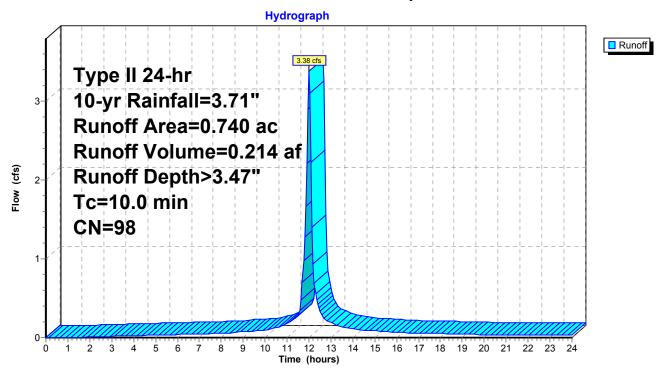
Printed 8/1/2018 Page 6

#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 3.38 cfs @ 12.01 hrs, Volume= 0.214 af, Depth> 3.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 10-yr Rainfall=3.71"

_	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
_	0.	740		100.	00% Impe	rvious Area	
	Тс	Lengt	h :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·
	10.0						Direct Entry, Minimum TC



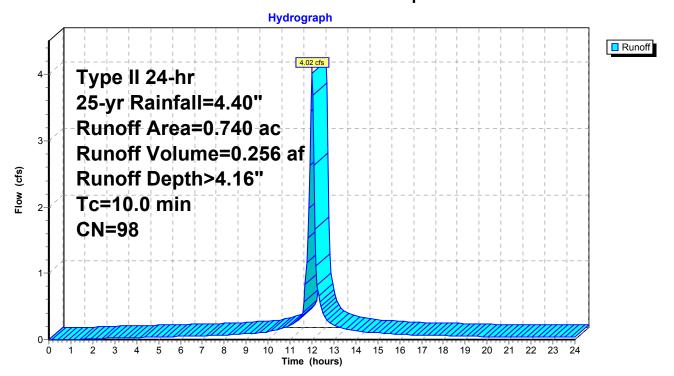
Printed 8/1/2018 Page 7

#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 4.02 cfs @ 12.01 hrs, Volume= 0.256 af, Depth> 4.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 25-yr Rainfall=4.40"

_	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
_	0.	740		100.	00% Impe	rvious Area	
	Тс	Lengt	h :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·
	10.0						Direct Entry, Minimum TC



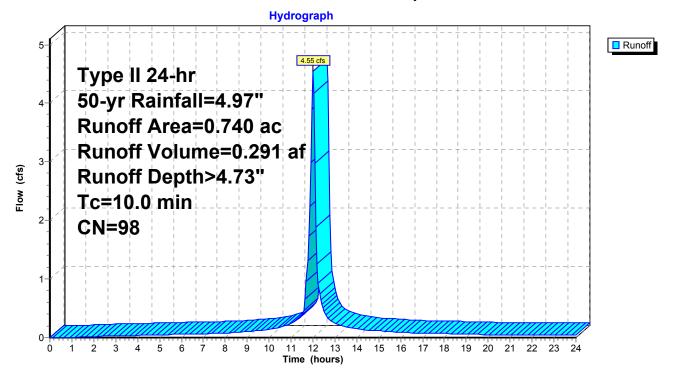
Page 8

#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 4.55 cfs @ 12.01 hrs, Volume= 0.291 af, Depth> 4.73"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 50-yr Rainfall=4.97"

_	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
_	0.	740		100.	00% Impe	rvious Area	
	Тс	Lengt	h :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·
	10.0						Direct Entry, Minimum TC



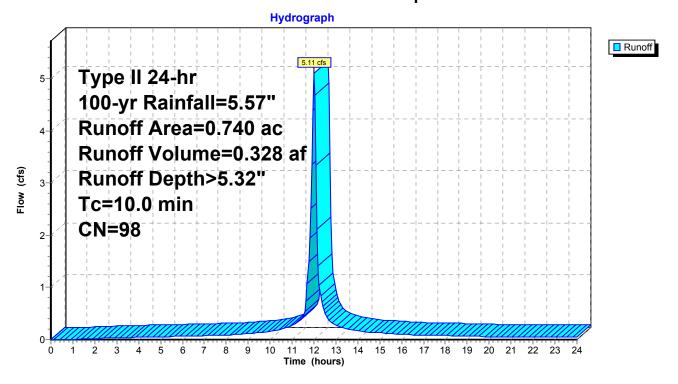
Page 9

#### **Summary for Subcatchment 2: Post-Development Area**

Runoff = 5.11 cfs @ 12.01 hrs, Volume= 0.328 af, Depth> 5.32"

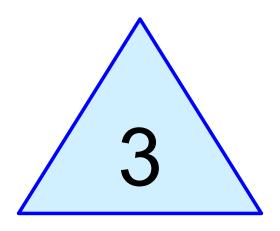
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type II 24-hr 100-yr Rainfall=5.57"

_	Area	(ac)	CN	Desc	cription		
*	0.	740	98	Impe	ervious		
_	0.	740		100.	00% Impe	rvious Area	
	Тс	Lengt	h :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·
	10.0						Direct Entry, Minimum TC





## **Appendix E – Routed Calculations**



# **Underground Detention**









Prepared by American Structurepoint

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Page 2

#### **Summary for Pond 3: Underground Detention**

Inflow Area = 0.740 ac,100.00% Impervious, Inflow Depth > 1.96" for 1-yr event

Inflow = 1.97 cfs @ 12.01 hrs, Volume= 0.121 af

Outflow = 1.20 cfs @ 12.11 hrs, Volume= 0.111 af, Atten= 39%, Lag= 6.3 min

Primary = 1.20 cfs @ 12.11 hrs, Volume= 0.111 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 931.46' @ 12.11 hrs Surf.Area= 0.041 ac Storage= 0.031 af

Plug-Flow detention time= 86.9 min calculated for 0.111 af (92% of inflow) Center-of-Mass det. time= 43.8 min ( 807.8 - 764.0 )

Volume	Invert	Avail.Storage	Storage Description
#1A	930.11'	0.041 af	27.50'W x 65.00'L x 4.00'H Field A
			0.164 af Overall - 0.063 af Embedded = 0.102 af x 40.0% Voids
#2A	930.61'	0.063 af	CMP Round 36 x 18 Inside #1
			Effective Size= 36.0"W x 36.0"H => 7.07 sf x 20.00'L = 141.4 cf
			Overall Size= 36.0"W x 36.0"H x 20.00'L
			6 Rows of 3 Chambers
			25.50' Header x 7.07 sf x 1 = 180.2 cf Inside
		0.103 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	930.61'	12.0" Round RCP_Round 12"
	Š		L= 23.0' RCP, rounded edge headwall, Ke= 0.100
			Inlet / Outlet Invert= 930.61' / 930.51' S= 0.0043 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
#2	Device 1	930.61'	10.0" W x 4.4" H Vert. Orifice/Grate C= 0.600
#3	Device 1	931.95'	<b>24.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600

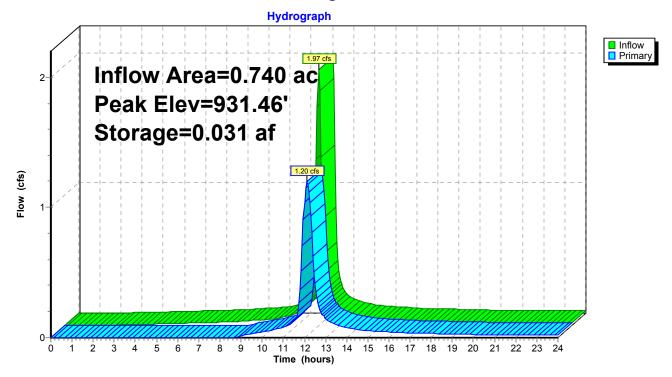
Primary OutFlow Max=1.19 cfs @ 12.11 hrs HW=931.46' (Free Discharge)

**\_1=RCP\_Round 12"** (Passes 1.19 cfs of 1.90 cfs potential flow)

**2=Orifice/Grate** (Orifice Controls 1.19 cfs @ 3.91 fps)

3=Orifice/Grate (Controls 0.00 cfs)

**Pond 3: Underground Detention** 



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#### **Summary for Pond 3: Underground Detention**

Inflow Area = 0.740 ac,100.00% Impervious, Inflow Depth > 2.39" for 2-yr event

Inflow = 2.37 cfs @ 12.01 hrs, Volume= 0.147 af

Outflow = 1.35 cfs @ 12.12 hrs, Volume= 0.137 af, Atten= 43%, Lag= 6.7 min

Primary = 1.35 cfs @ 12.12 hrs, Volume= 0.137 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 931.64' @ 12.12 hrs Surf.Area= 0.041 ac Storage= 0.037 af

Plug-Flow detention time= 78.4 min calculated for 0.137 af (93% of inflow)

Center-of-Mass det. time= 40.9 min (800.5 - 759.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	930.11'	0.041 af	27.50'W x 65.00'L x 4.00'H Field A
			0.164 af Overall - 0.063 af Embedded = 0.102 af x 40.0% Voids
#2A	930.61'	0.063 af	CMP Round 36 x 18 Inside #1
			Effective Size= 36.0"W x 36.0"H => 7.07 sf x 20.00'L = 141.4 cf
			Overall Size= 36.0"W x 36.0"H x 20.00'L
			6 Rows of 3 Chambers
			25.50' Header x 7.07 sf x 1 = 180.2 cf Inside
		0.400 - 5	Tatal Assallate Otamana

0.103 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	930.61'	12.0" Round RCP_Round 12"
	·		L= 23.0' RCP, rounded edge headwall, Ke= 0.100
			Inlet / Outlet Invert= 930.61' / 930.51' S= 0.0043 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
#2	Device 1	930.61'	10.0" W x 4.4" H Vert. Orifice/Grate C= 0.600
#3	Device 1	931.95'	24.0" W x 6.0" H Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=1.34 cfs @ 12.12 hrs HW=931.63' (Free Discharge)

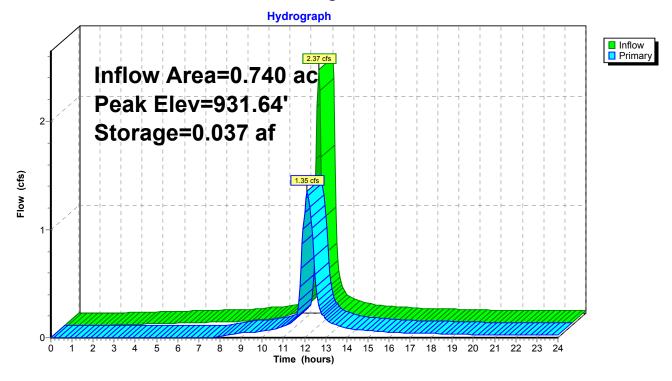
**—1=RCP\_Round 12"** (Passes 1.34 cfs of 2.52 cfs potential flow)

**2=Orifice/Grate** (Orifice Controls 1.34 cfs @ 4.40 fps)

**□3=Orifice/Grate** (Controls 0.00 cfs)

-

**Pond 3: Underground Detention** 



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#### **Summary for Pond 3: Underground Detention**

Inflow Area = 0.740 ac,100.00% Impervious, Inflow Depth > 2.98" for 5-yr event

Inflow = 2.93 cfs @ 12.01 hrs, Volume= 0.184 af

Outflow = 1.54 cfs @ 12.13 hrs, Volume= 0.174 af, Atten= 47%, Lag= 7.3 min

Primary = 1.54 cfs @ 12.13 hrs, Volume= 0.174 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 931.90' @ 12.13 hrs Surf.Area= 0.041 ac Storage= 0.045 af

Plug-Flow detention time= 69.6 min calculated for 0.174 af (95% of inflow)

Center-of-Mass det. time= 37.7 min ( 792.7 - 755.0 )

Volume	Invert	Avail.Storage	Storage Description
#1A	930.11'	0.041 af	27.50'W x 65.00'L x 4.00'H Field A
			0.164 af Overall - 0.063 af Embedded = 0.102 af x 40.0% Voids
#2A	930.61'	0.063 af	CMP Round 36 x 18 Inside #1
			Effective Size= 36.0"W x 36.0"H => 7.07 sf x 20.00'L = 141.4 cf
			Overall Size= 36.0"W x 36.0"H x 20.00'L
			6 Rows of 3 Chambers
			25.50' Header x 7.07 sf x 1 = 180.2 cf Inside
		0.402.5	Total Available Ctarage

0.103 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	930.61'	12.0" Round RCP_Round 12"
	·		L= 23.0' RCP, rounded edge headwall, Ke= 0.100
			Inlet / Outlet Invert= 930.61' / 930.51' S= 0.0043 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
#2	Device 1	930.61'	10.0" W x 4.4" H Vert. Orifice/Grate C= 0.600
#3	Device 1	931.95'	24.0" W x 6.0" H Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=1.54 cfs @ 12.13 hrs HW=931.89' (Free Discharge)

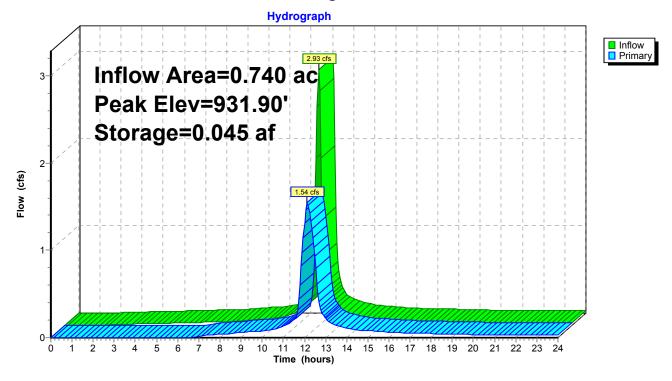
**—1=RCP\_Round 12"** (Passes 1.54 cfs of 3.25 cfs potential flow)

**2=Orifice/Grate** (Orifice Controls 1.54 cfs @ 5.03 fps)

3=Orifice/Grate (Controls 0.00 cfs)

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### **Pond 3: Underground Detention**



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#### **Summary for Pond 3: Underground Detention**

Inflow Area = 0.740 ac,100.00% Impervious, Inflow Depth > 3.47" for 10-yr event

Inflow = 3.38 cfs @ 12.01 hrs, Volume= 0.214 af

Outflow = 1.99 cfs @ 12.12 hrs, Volume= 0.204 af, Atten= 41%, Lag= 6.7 min

Primary = 1.99 cfs @ 12.12 hrs, Volume= 0.204 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 932.09' @ 12.12 hrs Surf.Area= 0.041 ac Storage= 0.051 af

Plug-Flow detention time= 63.5 min calculated for 0.203 af (95% of inflow) Center-of-Mass det. time= 35.4 min (787.5 - 752.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	930.11'	0.041 af	27.50'W x 65.00'L x 4.00'H Field A
			0.164 af Overall - 0.063 af Embedded = 0.102 af x 40.0% Voids
#2A	930.61'	0.063 af	CMP Round 36 x 18 Inside #1
			Effective Size= 36.0"W x 36.0"H => 7.07 sf x 20.00'L = 141.4 cf
			Overall Size= 36.0"W x 36.0"H x 20.00'L
			6 Rows of 3 Chambers
			25.50' Header x 7.07 sf x 1 = 180.2 cf Inside
	_	0.103 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	930.61'	12.0" Round RCP_Round 12"
	-		L= 23.0' RCP, rounded edge headwall, Ke= 0.100
			Inlet / Outlet Invert= 930.61' / 930.51' S= 0.0043 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
#2	Device 1	930.61'	10.0" W x 4.4" H Vert. Orifice/Grate C= 0.600
#3	Device 1	931.95'	<b>24.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600

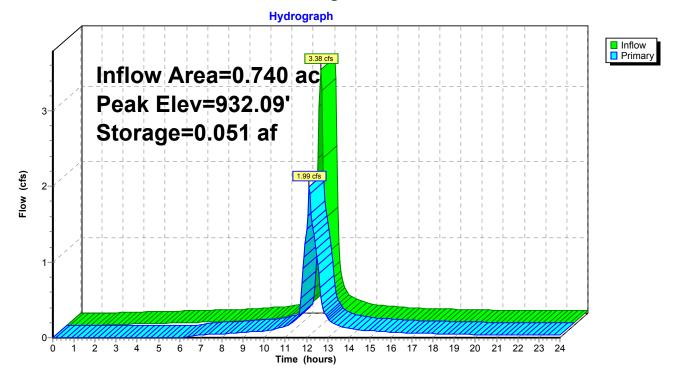
Primary OutFlow Max=1.94 cfs @ 12.12 hrs HW=932.07' (Free Discharge)

**—1=RCP\_Round 12"** (Passes 1.94 cfs of 3.72 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.66 cfs @ 5.44 fps)

-3=Orifice/Grate (Orifice Controls 0.28 cfs @ 1.13 fps)

**Pond 3: Underground Detention** 



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#### **Summary for Pond 3: Underground Detention**

Inflow Area = 0.740 ac,100.00% Impervious, Inflow Depth > 4.16" for 25-yr event

Inflow = 4.02 cfs @ 12.01 hrs, Volume= 0.256 af

Outflow = 2.85 cfs @ 12.10 hrs, Volume= 0.246 af, Atten= 29%, Lag= 5.6 min

Primary = 2.85 cfs @ 12.10 hrs, Volume= 0.246 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 932.25' @ 12.10 hrs Surf.Area= 0.041 ac Storage= 0.056 af

Plug-Flow detention time= 56.8 min calculated for 0.246 af (96% of inflow)

Center-of-Mass det. time= 32.3 min (781.1 - 748.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	930.11'	0.041 af	27.50'W x 65.00'L x 4.00'H Field A
			0.164 af Overall - 0.063 af Embedded = 0.102 af x 40.0% Voids
#2A	930.61'	0.063 af	CMP Round 36 x 18 Inside #1
			Effective Size= 36.0"W x 36.0"H => 7.07 sf x 20.00'L = 141.4 cf
			Overall Size= 36.0"W x 36.0"H x 20.00'L
			6 Rows of 3 Chambers
			25.50' Header x 7.07 sf x 1 = 180.2 cf Inside
		0.402.ef	Total Available Starage

0.103 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	930.61'	12.0" Round RCP_Round 12"
	-		L= 23.0' RCP, rounded edge headwall, Ke= 0.100
			Inlet / Outlet Invert= 930.61' / 930.51' S= 0.0043 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
#2	Device 1	930.61'	10.0" W x 4.4" H Vert. Orifice/Grate C= 0.600
#3	Device 1	931.95'	<b>24.0" W x 6.0" H Vert. Orifice/Grate</b> C= 0.600

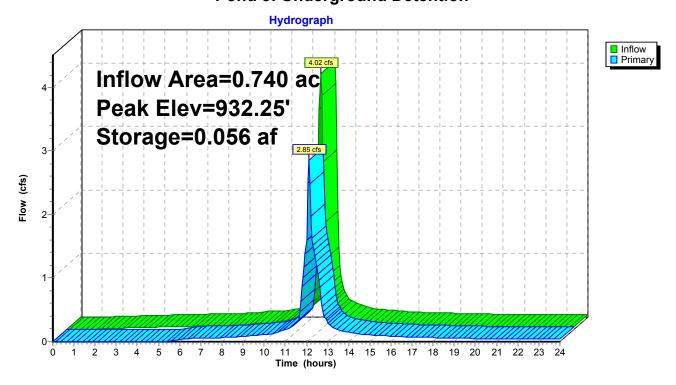
Primary OutFlow Max=2.84 cfs @ 12.10 hrs HW=932.25' (Free Discharge)

**—1=RCP\_Round 12"** (Passes 2.84 cfs of 4.27 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.78 cfs @ 5.81 fps)

-3=Orifice/Grate (Orifice Controls 1.07 cfs @ 1.76 fps)

**Pond 3: Underground Detention** 



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#### **Summary for Pond 3: Underground Detention**

Inflow Area = 0.740 ac,100.00% Impervious, Inflow Depth > 4.73" for 50-yr event

Inflow = 4.55 cfs @ 12.01 hrs, Volume= 0.291 af

Outflow = 3.49 cfs @ 12.09 hrs, Volume= 0.281 af, Atten= 23%, Lag= 4.8 min

Primary = 3.49 cfs @ 12.09 hrs, Volume= 0.281 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 932.36' @ 12.09 hrs Surf.Area= 0.041 ac Storage= 0.060 af

Plug-Flow detention time= 52.6 min calculated for 0.281 af (96% of inflow)

Center-of-Mass det. time= 30.2 min (776.8 - 746.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	930.11'	0.041 af	27.50'W x 65.00'L x 4.00'H Field A
			0.164 af Overall - 0.063 af Embedded = 0.102 af x 40.0% Voids
#2A	930.61'	0.063 af	CMP Round 36 x 18 Inside #1
			Effective Size= 36.0"W x 36.0"H => 7.07 sf x 20.00'L = 141.4 cf
			Overall Size= 36.0"W x 36.0"H x 20.00'L
			6 Rows of 3 Chambers
			25.50' Header x 7.07 sf x 1 = 180.2 cf Inside
		0.400.5	=

0.103 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	930.61'	12.0" Round RCP_Round 12"
	·		L= 23.0' RCP, rounded edge headwall, Ke= 0.100
			Inlet / Outlet Invert= 930.61' / 930.51' S= 0.0043 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
#2	Device 1	930.61'	10.0" W x 4.4" H Vert. Orifice/Grate C= 0.600
#3	Device 1	931.95'	24.0" W x 6.0" H Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=3.41 cfs @ 12.09 hrs HW=932.34' (Free Discharge)

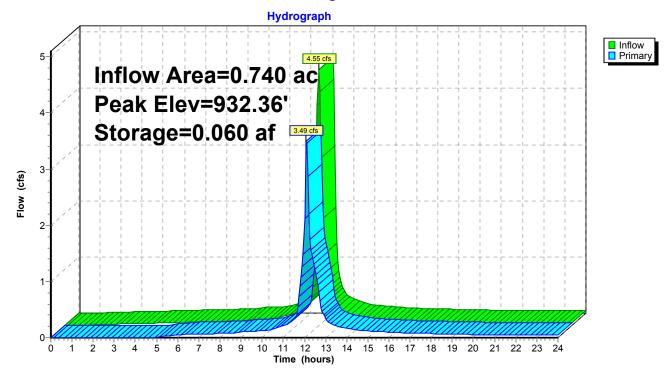
**—1=RCP\_Round 12"** (Passes 3.41 cfs of 4.52 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.83 cfs @ 5.99 fps)

-3=Orifice/Grate (Orifice Controls 1.58 cfs @ 2.01 fps)

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**Pond 3: Underground Detention** 



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#### **Summary for Pond 3: Underground Detention**

Inflow Area = 0.740 ac,100.00% Impervious, Inflow Depth > 5.32" for 100-yr event

Inflow = 5.11 cfs @ 12.01 hrs, Volume= 0.328 af

Outflow = 4.23 cfs @ 12.07 hrs, Volume= 0.318 af, Atten= 17%, Lag= 4.0 min

Primary = 4.23 cfs @ 12.07 hrs, Volume= 0.318 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 932.46' @ 12.07 hrs Surf.Area= 0.041 ac Storage= 0.063 af

Plug-Flow detention time= 48.5 min calculated for 0.317 af (97% of inflow)

Center-of-Mass det. time= 28.2 min (773.0 - 744.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	930.11'	0.041 af	27.50'W x 65.00'L x 4.00'H Field A
			0.164 af Overall - 0.063 af Embedded = 0.102 af x 40.0% Voids
#2A	930.61'	0.063 af	CMP Round 36 x 18 Inside #1
			Effective Size= 36.0"W x 36.0"H => 7.07 sf x 20.00'L = 141.4 cf
			Overall Size= 36.0"W x 36.0"H x 20.00'L
			6 Rows of 3 Chambers
			25.50' Header x 7.07 sf x 1 = 180.2 cf Inside
		- 100 -	

0.103 af Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	930.61'	12.0" Round RCP_Round 12"
	·		L= 23.0' RCP, rounded edge headwall, Ke= 0.100
			Inlet / Outlet Invert= 930.61' / 930.51' S= 0.0043 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf
#2	Device 1	930.61'	10.0" W x 4.4" H Vert. Orifice/Grate C= 0.600
#3	Device 1	931.95'	24.0" W x 6.0" H Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=4.08 cfs @ 12.07 hrs HW=932.44' (Free Discharge)

**—1=RCP\_Round 12"** (Passes 4.08 cfs of 4.78 cfs potential flow)

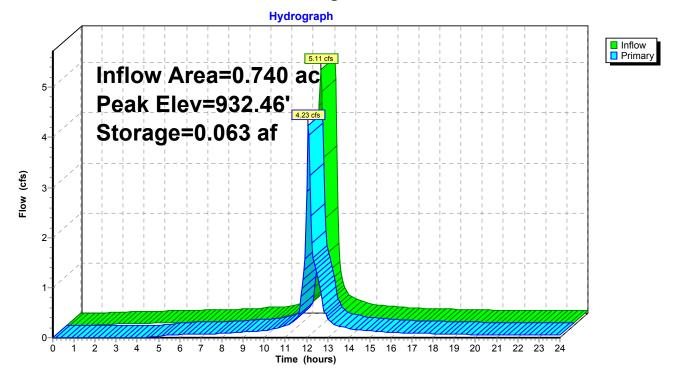
2=Orifice/Grate (Orifice Controls 1.89 cfs @ 6.17 fps)

-3=Orifice/Grate (Orifice Controls 2.19 cfs @ 2.24 fps)

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### **Pond 3: Underground Detention**





## **Appendix G – Storm Sewer Calculations**

#### STORM SEWER DESIGN CALCULATIONS

Project: Center Street Market 2018.00186

Job #: 2018.00186 Location: Hilliard, Ohio Date 08/11/18 Downstream of Underground Detention Outlet Control. Q is taken from HydroCAD Modeling for the 2-year design storm



Calc By: JRP Chk By:

Page 1 of 2

Date	08/11/18  Rain Fall Data  ODOT Zone D									2 Year Design Storm Manning Coefficient 0.013										Chk By:			
	Rain Fall Data									Manning Coefficient 0.013 Storm Sewer											BJM		
Ctructuro	COC				rainage Are	ea		I ime of	Conc. (Tc)	Desig	n Flow		<u> </u>	Storm	Sewer	Divis		lance and	1		tructures		
Structure #	Structure Type	Station	Tributary (acres)	Cumul. Tributary (acres)	С	CA	Cumul. CA	Tc (min)	Tc Cumul. <i>(min)</i>	Intensity (in/hr)	Design Q (cfs)	Length (ft)	Pipe Size (in)	Slope (%)	Velocity (ft/sec)	Pipe Capacity (cfs)	Status	Invert Up <i>(ft)</i>	Invert Down <i>(ft)</i>	Invert Drop (ft)	Rim Elev <i>(ft)</i>	Depth (ft)	Cover (ft)
UDS	Underground Detention System	0+27.42	0.74	0.74	0.98	0.73	0.73	10.00	10.00	4.16	1.35				OK								
												27.42	12	0.45	3.05	2.40	OK		930.63		934.55	3.92	2.75
1	Standard Curb & Gutter Inlets (AA-S125A)	0+00.00	0.00	0.74	0.98	0.00	0.73	0.15	10.15	4.14	3.00												
																		930.51	930.41	0.10	934.51	4.00	2.83
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#### STORM SEWER DESIGN HYDRAULIC GRADE LINE CALCULATIONS

Project: Center Street Market Job #: 2018.002

Job #: **2018.002**Location: **Hilliard, Ohio**Date 08/011/2018



Page 1 of 2

Calc By: JRP Chk By:

Date	08/011/20	18				5	Year Check	c Storm		Manning	Coefficient	0.013	<b>1</b> 13						Chk By: BJM
		Major I	Losses		Minor Losses								St	orm Structu	res	Hydraulic Grade Line			
Structure	Intensity (in/hr)	Design Q (cfs)		Major Loss	Inlet Type	Inlet Loss	Transition Type			Outfall Loss	Minor Losses	Total Losses	Invert Up (ft)	Invert Down (ft)	Rim Elev <i>(ft)</i>	0.8*D (ft)	Min/Maj Losses (ft)	HGL (ft)	Status
UDS	4.82	3.50	0.958	0.26	Solid	0	Straight	0.1	Open	0.1	0.20	0.46	(11)	(11)	(15)		(11)		
													930.63	930.63	934.55	931.43	931.32	931.43	OK
1	4.79	3.47	0.946	0.00	Grate	0.25	Straight	0.1	Open	0.1	0.45	0.45	202 -4	000.44	221-1	200 = 1			011
													930.51	930.41	934.51	930.51	930.86	930.86	OK
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